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Groundwater Recharge Estimation and Salinity Risk in Magra Plain (Algeria) Abdelmadjid Boufekane^{1*}, Djamel Maizi¹, Gianluigi Busico², Mohamed Meddi³

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Abstract

In this study, an approach for assessing groundwater recharge and identifying areas at risk of salinity pollution was developed in Magra Plain (Algeria). This approach is based on the hydraulic characteristics of the vadose zone, precipitation, evapotranspiration, and soil moisture, using the Hydrus-1D model. The groundwater recharge was estimated in relationship to the annual cumulative values of the soil's actual evaporation and actual transpiration, while the salinization was evaluated in relationship to the water content variation and salt dynamic in the soil profiles from September 2021 to August 2022. The results showed that the groundwater recharge of the Magra Plain varies from 3.81% to 6.19% of the total precipitation, the salinity risk of the aquifer is related to natural conditions due to climate change (temperatures, precipitation) and the thickness of a permeable layer (lithology). This modeling approach will provide an effective means of assessing the risks associated with irrigation with saline water in semi-arid regions.

Keywords: Groundwater recharge, Soil, Salinity, Hydrus-1D, Semi-arid region, Algeria.

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1. Introduction

Groundwater resources are considered the most important source of freshwater worldwide, particularly in arid and semi-arid regions, e.g. Algeria, due to the lack of water resources. Moreover, in such countries, the risk of soil and aquifer salinization is extremely increased due to the effect of climate changes on precipitation and temperature regimes, limiting the availability of drinking water (Chen et al., 2019; Panda et al., 2020). This risk becomes even higher especially in irrigation where the utilization of salty water for irrigation could exacerbate soil and groundwater salinization (Pulido-Bosch et al., 2018; Tomaz et al., 2020). So, the analysis of water salinity finalized its reduction and mitigation, and management become mandatory in many irrigated areas around the world (Ayars et al., 1999; Djoudi et al., 2023). The scenario is made even more problematic by the fact that the phenomenon of groundwater salinization could be exacerbated by anthropogenic endorheic pollution and over-exploitation of aquifers, leading to a deterioration in groundwater quality (Khezzani and Bouchemal, 2018; Mastrocicco et al., 2021).

In the aquifer system, the vadose zone can act as a filter, removing or decreasing the pollutant concentration, introduced into the subsoil such as fertilizers and pesticides (Elkayam et al., 2015; Gumiero et al., 2019; Rama et al., 2022). Moreover, the vadose media also include soil horizons where many biochemical and physical processes are responsible for pollutant degradation could occur (Amundson et al., 2007; Al-hamed et al., 2022). These depuration characteristics are mainly attributable to the high organic matter concentrations and clay contents, which can trigger pollutant biological degradation, transformation, and sorption (De Mastro et al., 2022; Ewis et al., 2022). Therefore, the vadose zone can effectively be considered a buffer zone, protecting the groundwater resources and the knowledge of its hydrogeological mandatory, so to correctly understand all the processes involved in groundwater pollution mitigation (Selker et al., 1996; Stephens, 1996).

Groundwater recharge also plays a key role in groundwater availability and quality. It is one of the main components of the hydrological cycle, and it is responsible for groundwater replenishment. Anyway, its amount greatly varies both in time and space according to several hydrogeological and climatic factors (Smerdon et al., 2010; Busico et al., 2021). In addition,

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the migration and transformation of pollutants in the unsaturated zone are mainly caused by the percolation of meteoric water and accompanying physical and chemical processes like adsorption-desorption and dissolution-precipitation reactions between pollutant and soil particles (Rama et al., 2022; Xue et al., 2023).

Consequently, a proper and reliable assessment of groundwater recharge becomes mandatory to correctly estimate water resource availability and to assess aquifer vulnerability to pollutants (Scanlon et al., 2002). Many methodologies could be utilized for this purpose; the most common include water balance (Afsari et al., 2022), hydrological modeling (Razack et al., 2019), water table evolution (Boufekane et al., 2022), and natural rainfall infiltration (Ntona et al., 2022). However, changes in the piezometry and groundwater quality can be caused by many factors. Certain changes are caused by human activities (overexploitation, anthropogenic pollution) (Salifu et al. 2017; Dişli 2018), and others occur because of natural phenomena (low rainfall, high evapotranspiration) (Gain et al., 2012; Wang et al., 2022).

Among these, groundwater and solute modeling allows the understanding of all those transport processes within the unsaturated zone (Tarawneh et al., 2021). They are the methods for the analysis of different pollution scenarios, allowing the adoption of the best management actions.

Today, several models (numerical and analytical models) have been developed to assess groundwater recharge and solute transfer in the unsaturated zone, such as DAISY (Hansen et al., 1990), TOUGH2 (Pruess, 1991), SHAW (Flerchinger et al., 1996), SWAP (Van Dam et al., 1997), HYDRUS-1D (Šimůnek et al., 1998a; Šimůnek et al., 1998b), UNSATH (Fayer, 2000), and COUP (Jansson and Karlberg, 2001).

Among these, the model of Hydrus-1D (Šimůnek et al., 2005) is one of the most widely used models despite the common drawbacks of all numerical models, such as lack of input data for proper calibration and validation procedure (Ma et al., 2023; Ramos et al., 2023). The model uses two main equations for the calculation of water movement (Richards's equation, 1931) and solute transport (advection-dispersion equation, 1961) which require an iterative implicit technique (Damodhara et al., 2006). The model also allows the simulation of water, heat, and solute transport in one, two, or three-dimensional variably saturated porous media (Saâdi et al., 2018).

In this scenario, the main goals of this study are to estimate the potential groundwater recharge and the salinization risk degree for groundwater under different natural conditions

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and to highlight the role of vadose zone buffer property for the aquifer system, using the Hydrus-1D model. Water, leaching in two soil profiles with different hydrological characteristics, will be simulated to understand how the recharge and salt concentration repond to geological and sediment characteristics. This study will offer new insight into irrigation water regulation in the Magra Plain (Algeria), providing sustainable agriculture and water development.

2. Materials and methods

2.1. Study area

The Magra plain is located in the east of M'Sila Province (Central High Plateaus of Algeria) (**Figure 1**). Three morphological units characterize the whole region: i) the Hodna Mountains, ii) the Magra Plain and iii) Soubella Valley. The area shows a flat topography with an average altitude of 567 m a.m.s.l. (Amroune, 2018) and geographically is located a few km from the Chott El Hodna (Salt Lake) and between eastern longitude $4^{\circ} 49' 45'' - 5^{\circ} 10' 30'' E$ and northern latitude $35^{\circ} 30' 00'' - 35^{\circ} 40' 30'' N$.

The climate is classified as semi-arid with low and irregular precipitations (around 210 mm/year) and an average temperature of 19 °C for the period 1969-2015 (Amroune et al., 2020). The climatic pattern in the area is characterized by a cool dry season (spring), followed by a hot dry summer, and recently by cold and very low rainy seasons (autumn and winter). According to the Thornthwaite (1948) method and for the period 1969-2015, the evapotranspiration, runoff, and infiltration in the region are 735 mm (350%), 10 mm (5%), and 12 mm (6%), respectively. Moreover, the agricultural water deficit due to groundwater abstraction is estimated to be around 690 mm distributed throughout the year (Amroune, 2018).

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Figure 1. Location of the Magra Plain and geological map (Guiraud, 1970).

This plain is drained by two wadis (Ennfida Wadi and Soubella Wadi), flowing southward and feeding one of the largest Chott in Algeria (Chott El Hodna-Sebkhat) that are ephemeral salt lakes, present in the Saharan region of Africa.

Cereal crops, whose development and extension are highly dependent on the availability of water resources in sufficient quantity and quality, mainly represent agriculture. Groundwater is the main resource in this region.

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2.2. Magra plain's soils and layers lithology

The Magra Plain is characterized by the presence of black soils derived from alluvial parent material with a clay loam or silty clay loam texture (Madani, 2023). The soils are characterized as follows:

- Mountainous area (located in the north): here the Calcaric regosols are the most diffuse soils, even though they are very little developed due to the higher slope. They have a shallow, medium to fine-grained, unconsolidated parent material, possibly alluvial in origin, and no significant soil horizon and often show accumulations of calcium carbonate or gypsum.

- Central and South area: the Isohumic soils are present and are more evolved than in the mountainous area. Moreover, approaching the Chott El Hodna (South), the soils are affected by salts.

Two profiles, belonging to the plain, were selected. The dataset of the two profiles was collected and assembled during a geotechnical study which was carried out in the area of the two profiles (Nd and Sd profiles) to a depth of 25 meters, in October-December 2021. The first is located in the northern agricultural perimeters, and the second is located in the southern part. Both profiles are characterized by direct infiltration toward the surface water table (**Figure 1**). More precisely, the Nd profile, located in the north, has a sandy-clay texture throughout its depth (25 meters). Its dry residue varies between 1 and 2 gL⁻¹ (average value of 1.5 gL⁻¹). On the other hand, the Sd profile, located to the south, is marked by a sandy texture over its entire depth (25 meters). Its dry residue varies between 2 and 4 gL⁻¹ (average value of 3 gL⁻¹).

2.3. Geology and Hydrogeology

According to Flandrin (1951), Bertraneu (1955), Guiraud (1969), and Sonatrach (2005) (Amroune et al., 2017), different geological formations characterize the study area and are described below chronologically (**Figure 1**).

- The Triassic formations, appearing diapirs from (gypsum and clay), outcrop in the northeast of the region.

- The Jurassic formations made of carbonate facies (limestone and dolomite) form part of the reliefs of Hodna Mountains in the northeast of the region.

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- The Cretaceous formations are made of impermeable bedrock such as sandstone, clay, limestone, dolomite, and marl and form part of the reliefs of the Hodna Mountains in the northeast.

- The Eocene formations consist of fractured limestone representing the karstic aquifer in the North of the region.

- The Oligocene deposits consist of flint limestone and impermeable bedrock which characterize the North of the region.

- The Miocene deposits are essentially made of sandy clay, sandstone, and marl forming the major aquifer of the area, which occupies most of the plain.

- The Plio-Quaternary deposits are mainly formed by sand, gravel, conglomerate, silt, clay, loam, and gypsum. They represent a very productive aquifer, operated by small wells and boreholes (maximum depth: 150 meters), located in the east and south of the region.

In the southwest region, a natural outlet of the plain is observed; it is the Chott El Hodna (Sebkhat) that receives all surrounding surface waters. This Chott acts as a drainage system for water from the floods in the Magra Plain. This area also shows important salt deposits within geological formations.

Hydrogeologically, a complex multiple aquifer characterizes the study area. It is made up of two hydrogeological units:

- The first aquifer, hosted in the Eocene formations and made of fractured limestone (karstic aquifer), characterizes the north of the region.

- The second aquifer, the object of this study hosted in the Mio-Plio-Quaternary formations, is an unconfined aquifer, made of heterogeneous alluvium sediments. This aquifer represents the most important aquifer in the Magra Plain, and several wells and boreholes exploit it with depths not exceeding 80 meters.

According to the data of the National Resources Water Agency (ANRH) during the dry season of 2012, the piezometric level varies from 200 m in the South and up to 600 m in the North. The general groundwater flow is oriented from the northern side (Hodna Mountains) towards Chott El Hodna (Sebkhat) to the southwest side and it is mainly recharged for meteoric water. The large Chott (Sebkhat) is the natural outlet for groundwater.

Hydraulic conductivity varies from 2×10^{-2} to 7×10^{-2} m/s while transmissivity ranges between 5×10^{-3} and 8×10^{-3} m²/s and aquifer thickness varies between 150 and 300 m

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(Grine, 2009). However, the hydraulic gradient ranges between 2.3×10^{-3} and 8.1×10^{-3} (Grine, 2009), where the discharge water from the Hodna Mountains flows into the Magra plain, during the winter period or the flood events.

2.4. Hydrus-1D model simulation

2.4.1. Hydrus-1D model presentation

Hydrus-1D is a process-based model widely used in water and soil systems to simulate water flow, solute transport, and moisture distribution. The model was developed at California University (Šimůnek et al., 2006) to simulate the effects of irrigation on water and soil chemistry (Azhdari, 2008).

Several studies were performed worldwide, such as the United States (Šimůnek et al., 1998b; Šimůnek et al., 2005), Sweden (Gladnyeva and Saifadeen, 2012), Iran (Tafteh and Sepaskhah, 2012), China (He et al., 2017), India (Sangita et al., 2018), and Tunisia (Kanzari et al., 2018).

The Hydrus-1D model can simulate the one-dimensional water flow, heat, and solute transport in variably saturated soils (Šimůnek et al., 2006) in steady or transient regimes, using several metric systems and multiple time steps. This model is based on the Richards equation as well as the advection-dispersion equations in the case of water flow and solute transport, respectively.

Hydrus-1D solves the modified Richards' equation by eliminating the term that reflects water uptake by the roots, so that the mathematical expression for the Richards' equation will be (Šimůnek et al., 2006):

$\frac{\partial \theta}{\partial t} = \frac{\partial}{\partial z} \left[K \left(\frac{\partial h}{\partial z} + 1 \right) \right]$

where:

h Water pressure head [L], θ Volumetric water content [L³ L³], K unsaturated hydraulic conductivity [LT⁻¹], t the time, z the spatial coordinate.

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The equations of Mualem and Van Genuchten (MVG) (1980) (Van Genuchten, 1980; Mualem, 1976) are used to develop the water retention curve (θ (h)). The latter relates the volumetric water content in the pressure potential to the hydraulic conductivity curve (K(h)), as a function of its saturation state measured by h. The retention curve represented by the equation of van Genuchten (1980) is:

$$\theta(\mathbf{h}) = \begin{array}{c} \theta_{\mathbf{r}} + \frac{\theta_{\mathbf{s}} - \theta_{\mathbf{r}}}{1 + |\alpha \mathbf{h}^{n}|^{m}} & \mathbf{h} < 0\\ \theta_{\mathbf{s}} & \mathbf{h} \ge 0 \end{array}$$
 Where: $\mathbf{m} = 1 - \frac{1}{n}, n > 1$

Where:

- θ_r is the residual water content [L³ L⁻³], θ_s is the saturated water content [L³ L⁻³],
- h is the water pressure head [L],
- α [L⁻¹] and n are shape parameters.

The MVG equation where used for describing the hydraulic conductivity is:

$$X(h) = \frac{K_{s}rS_{e}^{1/2} \left[1 - \left(1 - S_{e}^{1/m}\right)^{n}\right]^{2}}{k < 0} \quad h < 0$$

With:

$$m = 1 - \frac{1}{n} n > 1$$
 and $S_e = \frac{\theta - \theta_r}{\theta_s - \theta_r}$,

 K_s the saturated hydraulic conductivity [LT⁻¹],

S_e the effective saturation [-],

r the pore connectivity parameter [-] equal to 0.5.

The equation that governs the solute transport in a variably saturated soil is the advectiondispersion equation, defined in Hydrus-1D as:

$$\frac{\partial \rho S}{\partial t} + \frac{\partial \theta C}{\partial t} = \frac{\partial}{\partial z} \left\{ \theta, D \frac{\partial C}{\partial z} \right\} - q \frac{\partial C}{\partial z}$$

Where:

z the spatial coordinate,

C and S solute concentrations in the liquid [ML⁻³] and solid [MM⁻¹] phases,

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S = KdC where Kd $[L^3M^{-1}]$ the partition coefficient,

q the volumetric flux density [LT⁻¹],

D the dispersion coefficient $[L^2T^{-1}]$,

 ρ the bulk soil density [ML⁻³].

2.4.2. Boundary and initial conditions

The initial condition along with boundary conditions were considered a 25 m deep vertical soil profile:

- In the case of the solute transport, the boundary conditions were coincident with the observed values of groundwater salinity.

- In the case of recharge, the upper boundary coincides with the atmospheric limit condition with surface runoff, whereas the lower boundary condition has been taken as free drainage.

At the soil surface, the reference evapotranspiration was calculated via the Penman-Monteith model, with the daily values of maximum and minimum temperature, precipitation, average humidity, and wind speed.

The Van Genuchten hydraulic parameters (θ_r , θ_s , α , n, and K_s), were calculated using the evaporation method and the hydraulic parameter values were calculated in the calibration phase.

The lower boundary condition corresponds to deep drainage where the release rate q (n), at the base of the soil profile at node n is considered as a component of the water table position (Hopmans and Stricker, 1989):

 $q(n) = q(h) = -A_{qh} \exp(B_{qh} | h - GWL0L |)$

With:

q(h) is the discharge rate [cm day⁻¹],

h is the pressure head at the bottom of the soil profile [cm],

 A_{qh} and B_{qh} are empirical parameters in [cm day⁻¹] and [cm⁻¹] respectively,

GWL0L is the reference groundwater depth [cm].

Vertical drainage across the lower boundary of the soil profile, in this case, is approximated by a flux that depends on the water table level.

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The rate for each year daily and a total period of two years (2016-2022) was simulated. The simulation for the total period corresponds to the period between the occurrence of the first and the last rainfall event of the considered year.

2.4.3. Climate data

Data period six years from the M'Sila meteorological station were collected (from 1 September 2016 to 31 August 2022). Figures 2, 3, and 4 show the data, used in the Penman-Monteith model: monthly variations of rainfall data, average values of maximum and minimum temperatures, average wind speed, and humidity, respectively.



Figure 2. Average rainfall variations during the period September 2016 to August 2022.



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Figure 3. Daily average values of maximum and minimum temperatures during the period September 2016 to August 2022.





2.4.4. Groundwater recharge

The main results, estimated by Hydrus-1D, are actual soil evaporation, actual transpiration, and groundwater recharge. The simulated piezometric level is assumed to be at a depth where the pressure head (h) is equal to 0. The assumption of a 1:1 gradient between h

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(pressure head) and z (soil depth) was checked to be valid for the present simulations (Leterme et al., 2012).

2.4.5. Hydrus-1D input parameters

The Rosetta model was used to define the soil hydraulic parameters (Schaap et al., 2001). The factors of the water flow, i) saturated water content (θ_s), ii) residual water content (θ_r), iii) inverse of the air entry value (α), iv) pore size distribution index (n), v) saturated hydraulic conductivity (K_s), vi) the pore connectivity parameter for two different soil layers, were calculated using the soil texture and the measured bulk density. The core sampling method was used to determine the bulk density. The international pipette method was considered for the particle size distribution.

The calibration process allowed the estimation of soil hydraulic parameter values. In this study, the simulations were conducted for 730 days with a daily scale. It was carried out on silty and sandy soils that can be considered representative of the study area. For solute transport parameters, concentration flux was used as both the upper and the lower boundary conditions; it is calculated in the laboratory. **Table 1** presents the soil hydraulic parameters, the Geometry information, and the solute transfer properties.

D ()	(-	(-	(-	(-	(-	Valu	ues	(-	
Parameters	N. P.F.S.	N.P.	N. P. S.	1 K	Nd profile	N. A. L.	Sd	profile	VPD
Geometry information	PRESS,	RESC	RESC	PRESS,	PAESS,	PRESS	PRESS,	PRESS,	PRESS
Depth (m)	N	N	N	N	≈25 1	N	N	25	Ň
Time information	PRESS	PAESS	PAESS	PRESS	I SAFE	PRESS	PRESS	I PARS	Po.
Simulation time (days)	PRESS	PRESS	PRESS	PRESSI	730	PRESS	PRESSIN	730	PRESSIN
Hydraulic properties	V	N.	V	V	V	V	V	V	N.
Layers (m) θ_r (cm ³ cm ⁻³) θ_s (cm ³ cm ⁻³) α (cm ⁻¹) n(-)	Mones Mones	IN PRESS MORES	M. PRESS M. PRESS	IN PRESS IN PRESS	0 - 25 0.065 0.42 0.07 0.51	M. PRESS M. PRESS	IN PRESS IN PRESS	0 – 25 0.075 0.54 0.75 0.89	IN PRESS IN POS.
K _s (cm.d ⁻¹) L Solute transfer proper	ties	RESS IN PRESS	RESS IN PRESS	RESS IN PRESS	1.60 0.5	RESS IN PRESS	RESS IN PRESS	2.46 0.5	RESS M. P.C.
Layer (m)	N.	N.	N	N.	0-25	N	×~ () - 25	N
Dispersion coefficient $K_d[M^{-1}L^3]$	[L] 3	V. PRESS	V PRESS	V PRESS	19 0	V.P.F.S.S	VPRESS	25 0	VPD
PESS I	PESS !!	PESS,	PESS,	PESS !!	LESS !!	PESS !!	PESS,	PESS !!	RESS.

 Table 1. Input parameters of Nd and Sd profiles.

Moreover, the observed values of groundwater salinity show the following:

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- For the Nd profile: the minimum and maximum values of water content were set to ($\theta = 0.1$ cm³cm⁻³) and ($\theta = 0.3$ cm³cm⁻³), respectively. The average value of dry residue is C = 1.5 g/L. - For the Sd profile: the minimum and maximum values of water content taken were set to ($\theta = 0.1$ cm³cm⁻³) and ($\theta = 0.3$ cm³cm⁻³), respectively. The average value of dry residue is C = 3

To resume, four different combinations in the model, representing different soil water contents and salt concentrations, were used to define the initial conditions (**Table 2**).

Table 2. Initial conditions of water content and solute concentration for Nd and Sd profiles.

V	8	8	8	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	8	8	8	N.	~ ~	~
Profiles	PESS	RESS	RESS	RESS	Nd profile	RES.	RESS	of Sd pro	ofile	RESS
Salt conce	ntrations	$: C'(gL^{-1})$	N	N	₹1.5	N	N	3.0	€ ÷	A.
Water con	tents: θ ($cm^3 cm^{-3}$)	2	0.1	8	0.3	S	0.1	<u>ي</u> 0.	.3
PAC.	PRE	PRE	PRE	PRE	PRE	PRE	PRE	PAL	PRE	PRE

2.5. Model calibration and validation

The robustness of the model was checked, using two approaches: graphical and statistical methods. For the first approach, measured and simulated volumetric water contents, groundwater recharge, and soil salinities were shown as a function of soil depth for the different time steps. The second approach is based on the calculation of the root mean square error (RMSE):

RMSE =
$$\sqrt{\frac{\sum_{i=1}^{n} (p_i - m_i)^2}{n}} X \frac{1}{\overline{m}} X 100$$

Where: n is the number of observations, m_i are the measured values, p_i are the predicted values, and \overline{m} is the average value of observed data.

The model was initialized for 730 days. The results of soil water and salt content were obtained at the 183th, 365th, 548th, and 730th days of simulation.

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3. Results and discussion

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3.1. Variations in water and salt content

3.1.1. Water content variation

According to the obtained results during the simulation period (730 days), the results of the simulation for the Nd profile are shown in **Figure 5**. In this case, the water content values vary between 0.110 cm³cm⁻³ and 0.150 cm³cm⁻³ at the ground surface: it slightly increases from 0 to 15 m while from 15 m to the bottom of the profile. It remains almost constant from 0.147 to 0.178 cm³cm⁻³. However, the simulated water content values are always lower than the initial conditions, highlighting the continuous dewatering of the unsaturated zone due to the existence of a layer of low permeability (clay layer) for the entire soil profile.

Figure 6 shows the result for the Sd profile where the water content values vary between $0.130 \text{ cm}^3 \text{ cm}^{-3}$ and $0.170 \text{ cm}^3 \text{ cm}^{-3}$ at the ground surface, showing progressively increases accordingly with the soil depth (bottom of the profile) varying between 0.207 and 0.265 cm³ cm⁻³.

Contrary to the Nd simulation, the Sd profile showed higher values of water content exceeding the initial conditions in some cases. This is probability due to the permeable nature of this soil (i.e.: sandy layer) which allows a greater infiltration of water after rain events.



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Figure 6. Variation of the water content for the Sd profile, for 730 days.

3.2.2. Salts content variation

As for the water content, the salt concentration trends obtained during the simulation period (730 days) showed similar results for all the combinations. According to the results shown in **Figure 7**, for the Nd profile, the concentration rate varies between 0.05 gL⁻¹ and 0.25gL⁻¹ at the ground surface. Moreover, it constantly increases until 0.69 gL⁻¹ moving downward remaining constant in the last 5 meters (from 15 m to 25 m, the bottom of the profile) where the final value is 0.72 gL⁻¹ after 730 days.

A general reduction in soil salinity, compared to the initial conditions (0.72 gL^{-1}) , was shown when simulating the salt content profiles. A continuous leaching of salt is noticed through the unsaturated zone due to the presence of clayey intercalations that are able to slow down the spread of salt. These results highlighted the general low contamination risk for groundwater located below this kind of soil.

According to the results, shown in **Figure 8**, for the Sd profile, the concentration rate ranged between 0.32 gL⁻¹ and 0.65 gL⁻¹ at the ground surface. It constantly increases from 0.51 gL⁻¹ to 0.94 gL⁻¹ from 0 to 15 m and from 15 m to 25 m (bottom of the profile). The trends of the profile change and gradually increase towards the final salt concentration of 1.87 gL⁻¹ after 730 days.

During the simulation period and under the initial conditions, the results of the variation of the solute concentration profiles showed the risk of high groundwater salinity in the area where the Sd profile is located. This can be explained by the presence of the sandy layer, which accelerates salt leaching into the aquifer and increases the salinity risk.

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Figure 8. Variation of the salt content for the Sd profile, $C = 3.0 \text{ gL}^{-1}$, for 730 days. 3.2.3. The calibration results of the Hydrus-1D model

The results of soil water and salt content were obtained at the 183th, 365th, 548th and 730th days of the simulation were presented in **Table 3** where the proposed model (Hydrus-1D) shows better performance in the prediction of soil water and salt content (the RMSE values are equal to 0).

S	S.	S.	S.	2	4	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	S.	E.	S.	27 - 27 27
N PA	N PR	N P	NP4	N PH	N D	Nd profile	Nd NI	NPH PH	Sd profile	Ya NI
PFESS	PRESS	PRESS	PRESS	PRES	PRESS	RMSE	PRESS	PRESS	RMSE	PRESS
	N.	N	N.	Ref WC	NV VV	SCV	SCV	Ren a	SCV	SCV
5	5	5	5	wc	. V	(1.5 gL^{-1})	(3.0 gL^{-1})	wcv	(1.5 gL^{-1})	(3.0 gL^{-1})
PAL	A. C.	PAR	A Star	L'H	PRE		P.F.	P. P.	A LE	Le L
N'S	N'S	N'S	N.S.	N'S	N'S	17	N'S	N S.W	N'S N'S	N.S.W.
E Star	PRE	PRE	PAR	A.	PRE		PAC	S. S	E E	Phillip Phillip

Table 3. Statistical evaluation (RMSE values) of the simulation results

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40, 24 A	1 L	Ph	Phillips	6	PR	Phillippe
183th days of simulation	0.0723	0.1234	0.1154	0.0815	0.1272	0.1306
365th days of simulation	0.0739	0.1265	0.1183	0.0826	0.1298	§ 0.1327
548th days of simulation	چ [®] 0.0754	0.1291	0.1211	0.0835	0.1316	0.1350
730th days of simulation	0.0776	0.1304	0.1238	₹ 0.0842 €	0.1332	0.1379

WCV: Water Content Variation SCV: Salt Content Variation

3.3. Modeling of the groundwater recharge

The Hydrus- 1D model was used to estimate the potential groundwater recharge in the study area for the period September 2021 to August 2022. Based on the research results of Leterme et al. (2012), the model was used to simulate groundwater recharge in relation to annual values of actual soil evaporation and transpiration. The Penman-Monteith model was used to calculate intercepted water evaporation, potential soil evaporation, and potential transpiration. These variables will be used in the Hydrus-1D model.

In the current simulation, the results (**Tables 4 and 5**) show, that in the North zone of the plain (Nd profile), the simulated groundwater recharge is equal to an average of 8 mm/yr coincident with the 3.81% of total rainfall, while the actual ET (ETa) is 93.24% of the potential ET (ET0). For the south zone of the plain instead), (Sd profile) the simulated actual groundwater recharge is around 13 mm/yr (6.19% of total rainfall), and the actual ET (ETa) is 94.42% of the potential ET (ET0).

Table 4. Average values of rainfall, potential groundwater recharge, potential actualevapotranspiration and potential reference evapotranspiration during the period September2021 to August 2022.

Zones of the plain	Rainfall (R)	Pot	ential Grou recharg	ndwater e	Pote	ential actu otranspirat (ETa)	al I tion & e	Potential reference evapotranspiration (ET0)		
North zone (Nd profile)	210	<u>ک</u>	8	24. 	<u>~mm/y</u>	<u>r s</u> 1021	2.W. S.	1095	S.	
South zone (Sd profile)	210	SIN PRE	13	SIN PRE	SIN PRE	1068	N N St	1131	SIN PRE	

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Figure 9 shows the potential groundwater recharge for the two soil profiles Nd and Sd during the period September 2021 to August 2022. The Magra plain is characterized by low annual precipitation (210 mm), and groundwater recharge shows almost no seasonality. The average groundwater depth, used for the numerical simulations, is 10 mm (8 to 13 mm). The higher monthly recharge was obtained in December, January, February, and March. According to these recharge values, it concluded that the monthly groundwater recharge values are related to the monthly climatic parameters (precipitation, temperature, and evaporation) (Boufekane et al., 2019) and to the lithology of the unsaturated zone (permeable or impermeable layer) (Boufekane et al., 2022).



Figure 9. Potential groundwater recharge from two profiles soils during the period September 2021 to August 2022.

Table 5. Average monthly values of simulated potential groundwater recharge during the
period September 2021 to August 2022.

5	5		8	5	<i>U</i> .	2	5	5		5	5		5	5	5	
SIN PR	SIN PR	SIN PO	Ċ	SAN PR	SIN PR	P	otenti	al Grou	ndwat	er rec	harge (r	nm)		SIN PR	SIN PR	
Mo	nth	IN PRE	Sep	Oct	Nov	Dec	Jan	Feb	Mar	Apr	Mai	Jun	Jul	Aug	Total Year)
Nd	profile	IN PO.	§ 0	0.1	1.0%	1.2	₫.5 ∛	1.1	1.4	<u>_</u> 0.7	0.5	0.4	0.1	Ø	8.0	
Sd	profile	V PRESS	0	§ 0.2	1.4	2.2	2.3	1.9	2.2	1.2	<u>_</u> 1.0	0.5	0.1	§ 0	13.0	

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In this semi-arid region, low-intensity rainfall does not play a very important role in groundwater recharge via infiltration and a considerable proportion of the precipitated water is lost via evaporation. Therefore, only torrential rains are capable of contributing to the groundwater supply.

The results of the simulation indicated that soil characteristics have a significant effect on soil water storage, and that the increasing use of irrigation amount could accelerate salt leaching as already stated also in different environments such as China (Zeng et al., 2014). Moreover, irrigation in agriculture significantly alters the water cycle, often with major environmental consequences, by increasing the salinity of recharge water from irrigated permeable soils and by recharging unconfined aquifers in drier regions such as Spain and South America (Foster et al., 2018).

4. Conclusion

In semi-arid regions like the Magra Plain (Algeria), salinization of groundwater due to intrinsic climatic characteristics, is a worrying issue to be managed and resolved. This study examined the interactions between the aquifer and the vadose zone to assess groundwater recharge and salinity risk. The main factors, influencing groundwater recharge salinity risk, are: rainfall, evaporation, soil nature, and vegetation.

The Hydrus-1D model was applied in the Magra plain. In the absence of soil layer information, except for texture, the approach, using combinations of initial conditions, is effective for predicting groundwater quality in the case of direct recharge. The results highlighted that the sandy layer accelerates infiltration towards the depths as well as the influence of water dynamics in the vadose zone. Conversely, the existence of clay intercalations in the unsaturated zone slows down the transit of water towards the aquifer (providing a good protection for groundwater). The sandy layer increases the salinity risk to the aquifer while the existence of clay intercalations in the unsaturated zone protects the groundwater. The recharge estimated during the period September 2021 to August 2022 varied from 8 to 13 mm (3.81% to 6.19% of total rainfall). The highest potential recharge was found for sandy clay and the lowest one for sandy soils. In addition, the decline in rainfall, the increase in temperature and evaporation will continue to threaten the groundwater resources (quantity and quality).

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Finally, according to Hydrus-1D model results, as recommendations to improve this study, additional scenarios, including multi-factorial analysis study of rainfall, evaporation and groundwater recharge, and longer-term simulations, need to be considered to increase results reliability. Moreover, this elaboration can give useful insight to minimize the risks of groundwater overexploitation and salinity, especially, in arid and semi-arid regions.

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